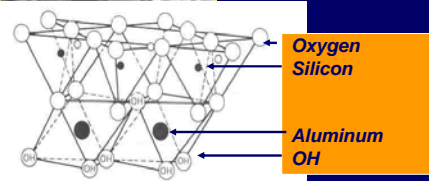


# Soil Basics

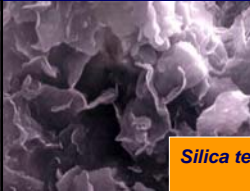


## SEM: Kaolinite

Surface area = 10 to 15 m<sup>2</sup>/g  
Surface Charge = 3 to 15 meq/100g



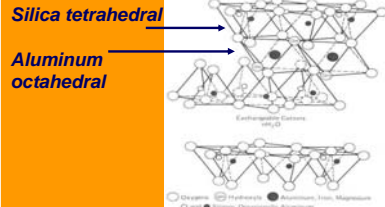
## SEM: Smectite



Surface area = up to 800 m<sup>2</sup>/g

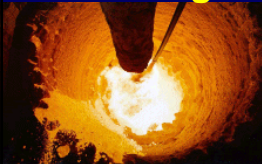
Surface charge = 100 meq/100g

Surface charge due to IS Al<sup>3+</sup> for Si<sup>4+</sup> or Mg<sup>2+</sup> for Al<sup>3+</sup>



# Lime Basics

## Calcining lime in rotary kiln



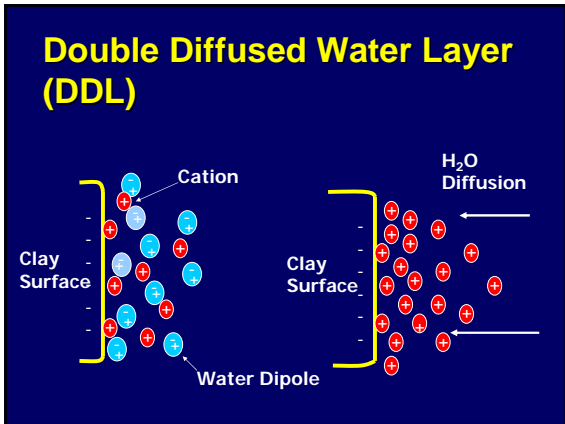
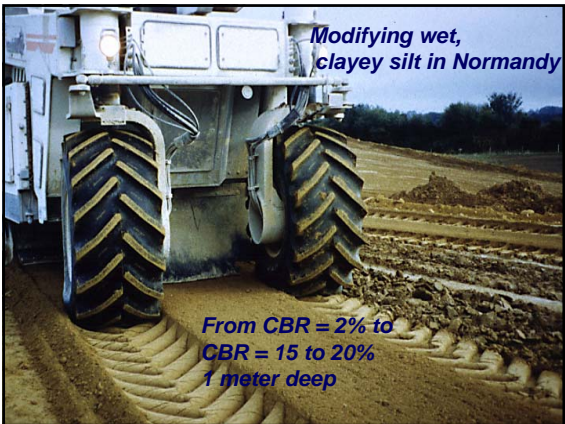
CaO



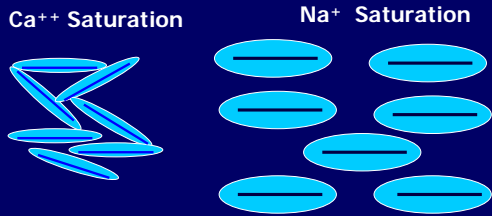
Ca(OH)<sub>2</sub>



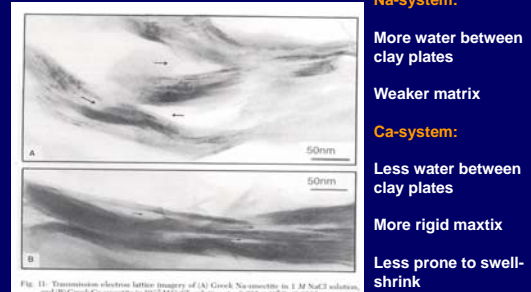
# Reactions



## Effect of Cation Adsorption on Attracted Water Layer



## TELI of (a) Na-Smectite 1 M NaCl; (b) Ca-Smectite 10<sup>-3</sup> M CaCl (near saturation)



**Na-system:**

More water between clay plates

Weaker matrix

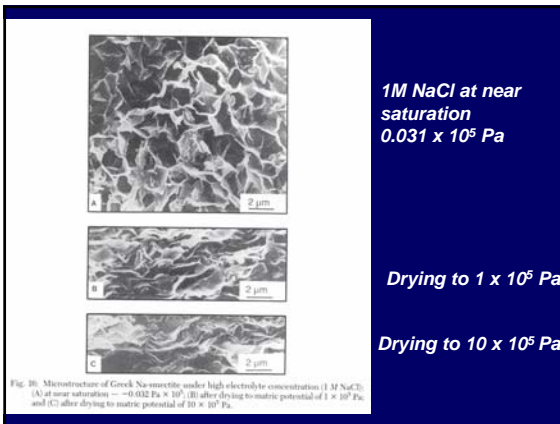
**Ca-system:**

Less water between clay plates

More rigid matrix

Less prone to swell-shrink

Fig. 11. Transmission electron lattice images of (A) Greek Na-smectite in 1 M NaCl solution and (B) Greek Ca-smectite in 10<sup>-3</sup> M CaCl<sub>2</sub> solution at -0.032 x 10<sup>5</sup> Pa. (0.032 bar suction; matrix potential for both). Note interparticle pores (arrows) between stacked clay particles.



**1M NaCl at near saturation**  
0.031 x 10<sup>5</sup> Pa

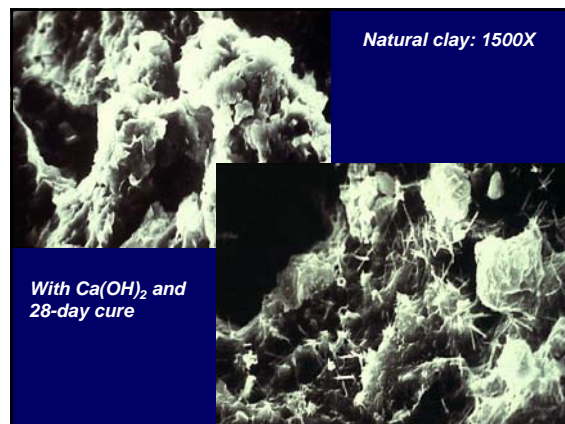
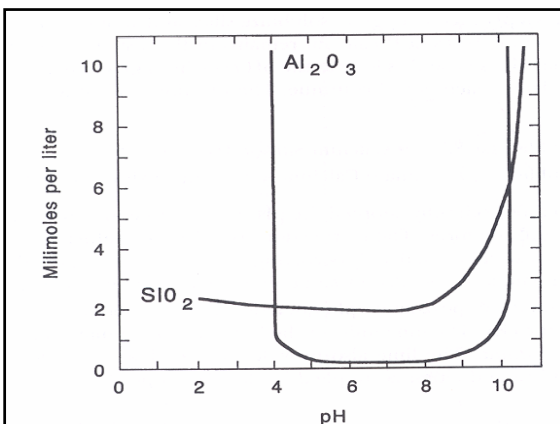
Drying to 1 x 10<sup>5</sup> Pa

Drying to 10 x 10<sup>5</sup> Pa

Fig. 10. Microstructure of Greek Na-smectite under high electrolyte concentration (1 M NaCl): (A) at near saturation (-0.032 Pa x 10<sup>5</sup>); (B) after drying to matrix potential of 1 x 10<sup>5</sup> Pa; and (C) after drying to matrix potential of 10 x 10<sup>5</sup> Pa.

## Pozzolanic Reaction

- High pH (> 12) environment when water added to CaO
- SiO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub> become soluble in high pH
- Ca<sup>++</sup> + SiO<sub>2</sub> + H<sub>2</sub>O = CSH
- Ca<sup>++</sup> + Al<sub>2</sub>O<sub>3</sub> + H<sub>2</sub>O = CAH

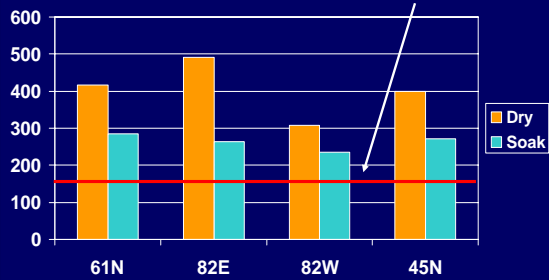


## Results

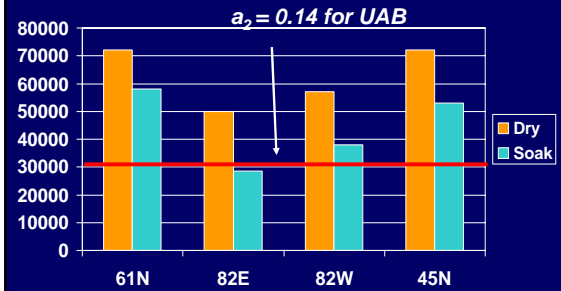
## Mississippi Pavements

Highway	HMA (in.)	Yrs of Service
US 45 N	10	17
US 61 N	12	15
US 82W	13	20
US 82E	10	20

## UCCS, psi (LSS) M.R. Thompson criteria, 1970



## Resilient Modulus, psi (LSS) $a_2 = 0.14$ for UAB



## Visual Analysis of Soak Testing



## Comparative Swell



## Field Data, DCP



Pavement	CBR, Subgrade (%)	CBR, LTS (%)	Ratio LTS: Subgrade
61N	15	200	33.3
82E	12	150	12.5
82W	4	47	11.8
45N	10	133	13.3

## Field Data, FWD



Pavement	Modulus, Subgrade (psi)	Modulus, LTS (psi)	Ratio LTS: Subgrade
61N	13,000	61,000	4.38
82E	17,000	352,000	20.72
82W	17,600	193,000	10.98
45N	17,900	211,000	11.86

## Field Data, GPR



Pavement	LTS Thickness	Dielectric Value
61N	150-mm	9 – 13
82E	150-mm	6 – 8
82W	150-mm	7 – 10
45N	250-mm	No Data

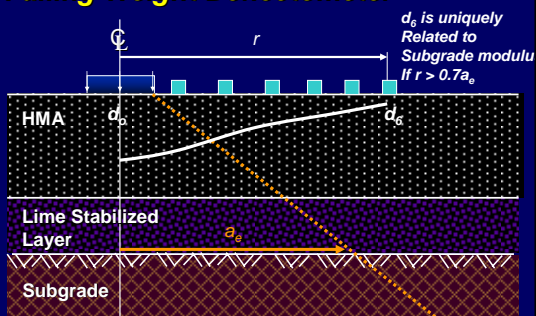
## The AASHTO Empirical Design Example "Statistically-Based" AASHTO Road Test



1958 – 1960  
Ottawa, Illinois

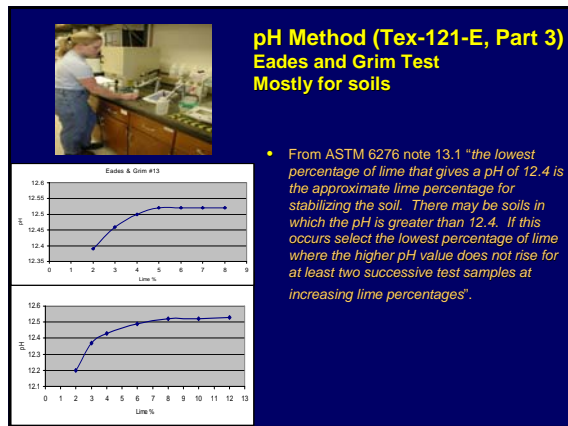
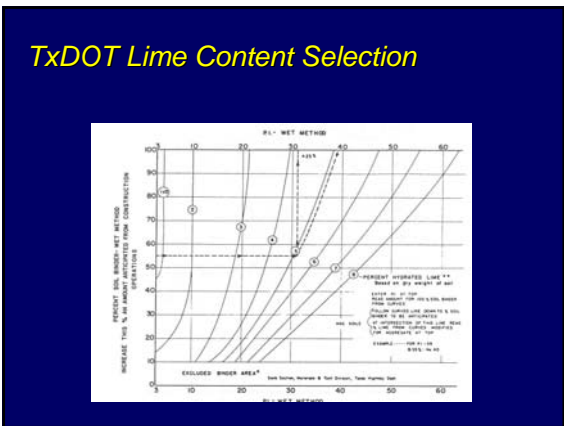
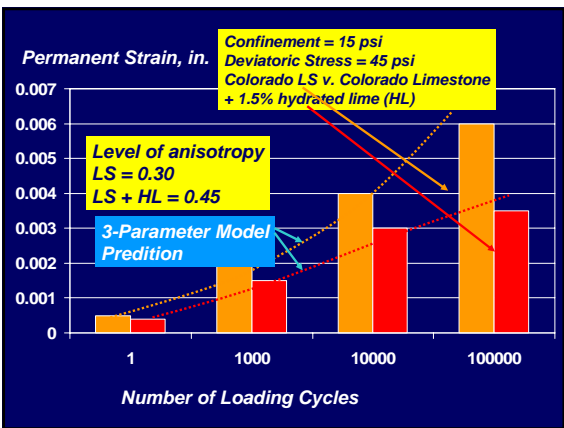
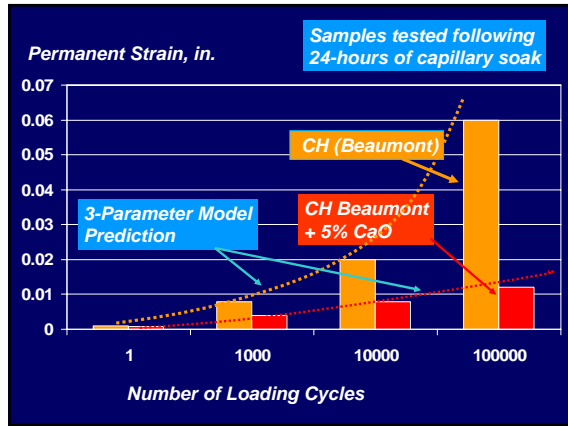
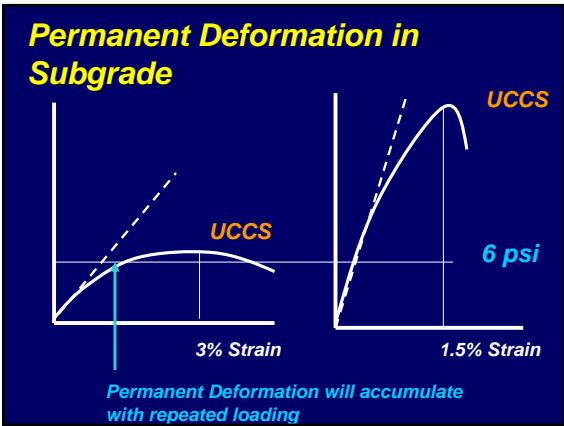
(AASHTO, 1961)

## Falling Weight Deflectometer



## Comparison of Design Values

Pavement	Lab UCCS, psi	Lab $M_R$ , psi	Field CBR, %	Field $a_2$
US 61N	285	50,000	200	0.13
US 82E	264	28,500	150	0.16
US 82 W	235	38,600	47	0.12
US 45N	271	53,000	133	0.14



## Soil-Lime Mix Design – Tex-121-E Part 1

- Minimum Strength Method
  - Develop M-D relationship in accordance to Tex-113-E
  - Mold 3 specimens (6 by 8") at varying percentages of lime
  - Place in triaxial cell and cure at room temp for 7 days
  - Remove cell, air dry at 140F for 6 hours (or loss 1/3 moisture)
  - Subject sample to capillary for 10 days
  - Determine the average UCS at each lime percent
  - Determine the minimum lime content the desired strength is achieved = Target Lime Content
  - Minimum UCS recommended for base is 150 psi and for subgrade is 50 psi



## National Lime Association Procedure (Little, 1998) – Yusuf, Little, & Sarkar, TRR 1757, pp. 22 – 31

- Step 1: Classify and assess suitability for lime stabilization
- Step 2: Perform Eades & Grim pH test (ASTM D 6276) to determine approximate optimum lime content
- Step 3: Determine moisture/density AASHTO T-99, TEX 113A) relationship for lime treated soil and determine strength gain following accelerated cure at approximate optimum lime content
- Step 4: Verify optimum lime content and determine unconfined compressive strength (UCCS – ASTM D 5102) following capillary soaking
- Step 5: Determine resilient modulus (Rapid Test or AASHTO T 307 – 99 at 6 psi deviatoric –  $Er\text{-ksi} = 0.124 (\text{UCCS-psi}) + 10$  following capillary soaking
- Step 6: Tube suction - discontinued

## Construction



Standard rubber-tire spreader equipped with an auger system and vane feeder for controlled dry product distribution.



Dry lime is spread with the distribution truck at the engineer's design rate of application.



The CMI RS-500B traveling rotary mixer is capable of uniformly blending lime and soil to a depth of 20 inches. The mixer is designed specifically for soil stabilization and asphalt pulverization. The CMI RS-500B is equipped with an on-board computer that controls the mixing depth and flow of water through the pump system.



The water truck is connected to the mixer as water is pumped through the mixer and into the soil for hydration of the lime. Note the degree of mixing after only one pass of the mixer. Initial mixing consists of two passes with the CMI RS-500B.



Water is a key ingredient in each stage of the lime stabilization process. Moisture is added to the lime treated soil after initial mixing and the soil is allowed to "mellow" in an uncompacted state overnight to allow for complete hydration of the lime and breakdown of the clay soil.



After the required mellowing period, the soil-lime mixture is remixed until gradation specifications are achieved and the material is uniform. The soil-lime mixture is moisture conditioned to achieve the specified moisture content prior to initial compaction.



Initial compaction is achieved with a Rex self-propelled padfoot compactor. The Rex compactor has the capacity to compact 12 inches of lime treated soil in-place. Typical specifications require 90 to 95 percent relative compaction.



The lime treated soil is then fine graded by the paving or grading contractor to within the paving elevation tolerances.



The lime treated soil is rolled with a smooth drum compactor in the "static" mode of the roller.

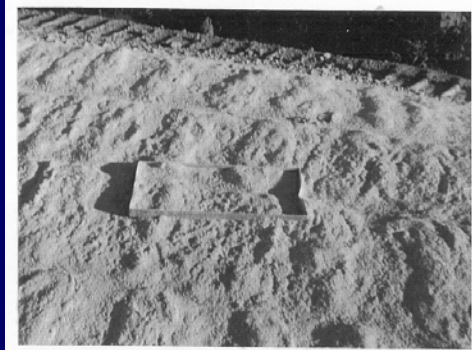




The lime treated soil after completion of final compaction with the smooth drum roller.



Engineers specify curing of the lime treated soil with asphalt emulsion, as seen above, or with periodic water applications - "moist cure" as seen below. Subsequent pavement layers, such as aggregate base or asphalt may now be placed over the lime treated layer.




**Depth of Treatment:**

Because lime elevates the pH of soil, phenolphthalein, a color-sensitive pH indicator solution, can be sprayed on the soil to indicate the presence of lime in the soil.

A trial test is performed on the natural or untreated soil by spraying the solution onto the soil. The soil will attain a deep pinkish color with a pH on the order of 10. Typically, there is no change in color with the application of the solution to the natural soil.


After an initial mix, the depth is measured by excavating a test pit through the lime treated layer and into the natural soil and spraying the solution along the face of the excavation. The depth of treatment can be measured directly or from survey stakes. Depth of mixing should be inspected periodically throughout the day.



**Degree of Pulverization:**

The phenolphthalein solution is again used to determine the degree of uniformity and pulverization. After final mixing, the solution is sprayed onto the soil-lime mixture and observations of the color changes are made. The presence of streaks or pockets of lime or non-uniformity of color reaction is considered evidence of inadequate mixing.

Alternatively, the degree of pulverization can be measured using selected sieve sizes. Most specifications are based on the 1 in. and the No. 4 sieve. The processed material is dry sieved to determine the percent passing.



**Density**

Conventional procedures, such as nuclear gage and sand cones are used to determine the in-place density of the compacted treated layer.

When dealing with lime stabilized soil, it is critical that the moisture density relations are determined from a field moist sample of the soil-lime mixture. The moisture density relations generally undergo changes consisting of reduced maximum dry densities and increased optimum moistures. These changes are also time dependent and may change relative to such factors as curing time.

Typically, in-place density is controlled relative to the wet density of the laboratory determined moisture density relation. Because moisture is a critical element in the soil stabilization process, testing by this method allows for relative compaction to be achieved at higher moisture contents.



**Moisture**

Conventional procedures such as oven dry and nuclear methods are used. Nuclear devices have a tendency to give higher moistures than the in-place moisture. As a result, moistures obtained from nuclear devices should be correlated to oven dry moistures and the device adjusted accordingly.



## Hydrated Lime Slurry

